## 650 kHz/1.2 MHz, 18.5 V STEP-UP DC-DC CONVERTER

Check for Samples: TPS61085

## FEATURES

- 2.3 V to 6 V Input Voltage Range
- 18.5 V Boost Converter With 2.0 A Switch Current
- 650 kHz/1.2 MHz Selectable Switching Frequency
- Adjustable Soft-Start
- Thermal Shutdown
- Undervoltage Lockout
- 8-Pin MSOP Package
- 8-Pin TSSOP Package


## APPLICATIONS

- Handheld Devices
- GPS Receiver
- Digital Still Camera
- Portable Applications
- DSL Modem
- PCMCIA Card
- TFT LCD Bias Supply


## DESCRIPTION

The TPS61085 is a high frequency, high efficiency DC to DC converter with an integrated $2.0 \mathrm{~A}, 0.13 \Omega$ power switch capable of providing an output voltage up to 18.5 V . The selectable frequency of 650 kHz or 1.2 MHz allows the use of small external inductors and capacitors and provides fast transient response. The external compensation allows optimizing the application for specific conditions. A capacitor connected to the soft-start pin minimizes inrush current at startup.


Please be aware that an important notice concerning availability, standard warranty, and use in critical applications of Texas Instruments semiconductor products and disclaimers thereto appears at the end of this data sheet.

These devices have limited built-in ESD protection. The leads should be shorted together or the device placed in conductive foam during storage or handling to prevent electrostatic damage to the MOS gates.
ORDERING INFORMATION ${ }^{(1)}{ }^{(1)}$

| $\mathbf{T}_{\mathbf{A}}$ | ORDERING | PACKAGE | PACKAGE MARKING |
| :---: | :---: | :---: | :---: |
| -40 to $85^{\circ} \mathrm{C}$ | TPS61085DGK | MSOP-8 (DGK) | PMKI |
| -40 to $85^{\circ} \mathrm{C}$ | TPS61085PW | TSSOP-8 (PW) | 61085 |

(1) The DGK and PW packages are available taped and reeled.
(2) For the most current package and ordering information, see the Package Option Addendum at the end of this document, or see the TI website at www.ti.com.

## ABSOLUTE MAXIMUM RATINGS

over operating free-air temperature range (unless otherwise noted) ${ }^{(1)(2)}$

|  | VALUE | UNIT |
| :--- | :---: | :---: |
| Input voltage range IN | -0.3 to 7 | V |
| Voltage range on pins EN, FB, SS, FREQ, COMP | -0.3 to 7 |  |
| Voltage on pin SW | -0.3 to 20 |  |
| ESD rating HBM | 2 | V |
| ESD rating MM | V |  |
| ESD rating CDM | See Dissipation Rating Table | kV |
| Continuous power dissipation | -40 to 150 | V |
| Operating junction temperature range | -65 to 150 | ${ }^{\circ} \mathrm{C}$ |
| Storage temperature range | ${ }^{\circ} \mathrm{C}$ |  |

(1) Stresses beyond those listed under absolute maximum ratings may cause permanent damage to the device. These are stress ratings only, and functional operation of the device at these or any other conditions beyond those indicated under recommended operating conditions is not implied. Exposure to absolute-maximum-rated conditions for extended periods may affect device reliability
(2) All voltage values are with respect to network ground terminal.

DISSIPATION RATINGS ${ }^{(1)(2)}$

| PACKAGE | $\mathbf{R}_{\text {日JA }}$ | $\mathbf{T}_{\mathbf{A}} \leq \mathbf{2 5}{ }^{\circ} \mathbf{C}$ <br> POWER RATING | $\mathbf{T}_{\mathbf{A}}=\mathbf{7 0} \mathbf{0}^{\circ} \mathbf{C}$ <br> POWER RATING | $\mathbf{T}_{\mathbf{A}}=\mathbf{8 5}{ }^{\circ} \mathbf{C}$ <br> POWER RATING |
| :---: | :---: | :---: | :---: | :---: |
| MSOP | $181^{\circ} \mathrm{C} / \mathrm{W}$ | 552 mW | 303 mW | 221 mW |
| TSSOP | $160^{\circ} \mathrm{C} / \mathrm{W}$ | 625 mW | 343 mW | 250 mW |

(1) $P_{D}=\left(T_{J}-T_{A}\right) / R_{\theta J A}$.
(2) $R_{\text {ӨJA. }}$. given for High-K PCB board.

## RECOMMENDED OPERATING CONDITIONS

|  |  | MIN | TYP | MAX |
| :--- | :--- | ---: | ---: | ---: |
| $\mathrm{V}_{\mathbb{I}}$ | UNIT |  |  |  |
| $\mathrm{V}_{\mathrm{S}}$ | Boost output voltage range | 2.3 | 6 | V |
| $\mathrm{~T}_{\mathrm{A}}$ | Operating free-air temperature | $\mathrm{V}_{\mathbb{I N}}+0.5$ | 18.5 | V |
| $\mathrm{~T}_{\mathrm{J}}$ | Operating junction temperature | -40 | 85 | ${ }^{\circ} \mathrm{C}$ |

## ELECTRICAL CHARACTERISTICS

$\mathrm{V}_{\mathrm{IN}}=3.3 \mathrm{~V}, \mathrm{EN}=\mathrm{V}_{\mathrm{IN}}, \mathrm{V}_{\mathrm{S}}=12 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=-40^{\circ} \mathrm{C}$ to $85^{\circ} \mathrm{C}$, typical values are at $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$ (unless otherwise noted)

| PARAMETER |  | TEST CONDITIONS | MIN | TYP | MAX | UNIT |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| SUPPLY |  |  |  |  |  |  |
| $\mathrm{V}_{\text {IN }}$ | Input voltage range |  | 2.3 |  | 6 | V |
| $\mathrm{I}_{\mathrm{Q}}$ | Operating quiescent current into IN | Device not switching, $\mathrm{V}_{\mathrm{FB}}=1.3 \mathrm{~V}$ |  | 70 | 100 | $\mu \mathrm{A}$ |
| ISDVIN | Shutdown current into IN | EN = GND |  |  | 1 | $\mu \mathrm{A}$ |
| UVLO | Undervoltage lockout threshold | $\mathrm{V}_{\text {IN }}$ falling |  |  | 2.2 | V |
|  |  | $\mathrm{V}_{\text {IN }}$ rising |  |  | 2.3 | V |
| $\mathrm{T}_{\text {SD }}$ | Thermal shutdown | Temperature rising |  | 150 |  | ${ }^{\circ} \mathrm{C}$ |
| $\mathrm{T}_{\text {SD(HYS }}$ | Thermal shutdown hysteresis |  |  | 14 |  | ${ }^{\circ} \mathrm{C}$ |
| LOGIC SIGNALS EN, FREQ |  |  |  |  |  |  |
| $\mathrm{V}_{\mathrm{IH}}$ | High level input voltage | $\mathrm{V}_{\mathrm{IN}}=2.3 \mathrm{~V}$ to 6 V | 2 |  |  | V |
| $\mathrm{V}_{\mathrm{IL}}$ | Low level input voltage | $\mathrm{V}_{\text {IN }}=2.3 \mathrm{~V}$ to 6 V |  |  | 0.5 | V |
| $\mathrm{l}_{\text {kg }}$ | Input leakage current | $\mathrm{EN}=\mathrm{FREQ}=\mathrm{GND}$ |  |  | 0.1 | $\mu \mathrm{A}$ |
| BOOST CONVERTER |  |  |  |  |  |  |
| $\mathrm{V}_{\mathrm{S}}$ | Boost output voltage |  | $\begin{array}{r} \mathrm{V}_{\mathrm{IN}}+ \\ 0.5 \end{array}$ |  | 18.5 | V |
| $\mathrm{V}_{\mathrm{FB}}$ | Feedback regulation voltage |  | 1.230 | 1.238 | 1.246 | V |
| gm | Transconductance error amplifier |  |  | 107 |  | $\mu \mathrm{A} / \mathrm{V}$ |
| $\mathrm{I}_{\text {FB }}$ | Feedback input bias current | $\mathrm{V}_{\mathrm{FB}}=1.238 \mathrm{~V}$ |  |  | 0.1 | $\mu \mathrm{A}$ |
| $\mathrm{r}_{\text {DS(on) }}$ | N-channel MOSFET on-resistance | $\mathrm{V}_{\mathrm{IN}}=\mathrm{V}_{\mathrm{GS}}=5 \mathrm{~V}, \mathrm{I}_{\text {SW }}=$ current limit |  | 0.13 | 0.20 | $\Omega$ |
|  |  | $\mathrm{V}_{\mathrm{IN}}=\mathrm{V}_{\mathrm{GS}}=3.3 \mathrm{~V}, \mathrm{I}_{\mathrm{SW}}=$ current limit |  | 0.15 | 0.24 |  |
| $\mathrm{I}_{\text {kg }}$ | SW leakage current | $\mathrm{EN}=\mathrm{GND}, \mathrm{V}_{\text {SW }}=6 \mathrm{~V}$ TBD |  |  | 10 | $\mu \mathrm{A}$ |
| ILIM | N-Channel MOSFET current limit |  | 2.0 | 2.6 | 3.2 | A |
| Iss | Soft-start current | $\mathrm{V}_{\text {SS }}=1.238 \mathrm{~V}$ | 7 | 10 | 13 | $\mu \mathrm{A}$ |
| $\mathrm{f}_{\mathrm{S}}$ | Oscillator frequency | FREQ $=\mathrm{V}_{\text {IN }}$ | 0.9 | 1.2 | 1.5 | MHz |
|  |  | FREQ = GND | 480 | 650 | 820 | kHz |
|  | Line regulation | $\mathrm{V}_{\text {IN }}=2.3 \mathrm{~V}$ to $6 \mathrm{~V}, \mathrm{I}_{\text {OUT }}=10 \mathrm{~mA}$ |  | 0.0002 |  | \%/V |
|  | Load regulation | $\mathrm{V}_{\text {IN }}=3.3 \mathrm{~V}$, $\mathrm{I}_{\text {OUT }}=1 \mathrm{~mA}$ to 400 mA |  | 0.11 |  | \%/A |

## PIN ASSIGNMENT

DGK, PW PACKAGES
(TOP VIEW)


8-PIN $4.9 \mathrm{~mm} \times 3 \mathrm{~mm} \times 1.1 \mathrm{~mm}$ MSOP (DGK) 8 -PIN $6.4 \mathrm{~mm} \times 3 \mathrm{~mm} \times 1.2 \mathrm{~mm}$ TSSOP (PW)

## PIN FUNCTIONS

| PIN |  | I/O |  |
| :--- | :---: | :---: | :--- | :--- |
| NAME | NO. |  |  |
| COMP | 1 | I/O | Compensation pin |
| FB | 2 | I | Feedback pin |
| EN | 3 | I | Shutdown control input. Connect this pin to logic high level to enable the device |
| PGND | 4 |  | Power ground |
| SW | 5 |  | Switch pin |
| IN | 6 |  | Input supply pin |
| FREQ | 7 | I | Frequency select pin. The power switch operates at 650 kHz if FREQ is connected to GND and at 1.2 MHz if <br> FREQ is connected to IN |
| SS | 8 |  | Soft-start control pin. Connect a capacitor to this pin if soft-start needed. Open = no soft-start |

TYPICAL CHARACTERISTICS

## TABLE OF GRAPHS

|  |  |  | FIGURE |
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The typical characteristics are measured with the inductors $74477890033.3 \mu \mathrm{H}$ (high frequency) or B82464G4 $6.8 \mu \mathrm{H}$ (low frequency) from Epcos and the rectifier diode SL22.


Figure 1.


Figure 3.

MAXIMUM LOAD CURRENT
vs
INPUT VOLTAGE


Figure 2.


Figure 4.


Figure 5.


Figure 7.

PWM SWITCHING CONTINUOUS CONDUCTION MODE


Figure 6.


Figure 8.


Figure 9.
FREQUENCY
vs
LOAD CURRENT


Figure 11.

SUPPLY CURRENT
vs
SUPPLY VOLTAGE


Figure 10.
FREQUENCY
vs
SUPPLY VOLTAGE


Figure 12.

## DETAILED DESCRIPTION



Figure 13. Block Diagram
The boost converter is designed for output voltages up to 18.5 V with a switch peak current limit of 2.0 A minimum. The device, which operates in a current mode scheme with quasi-constant frequency, is externally compensated for maximum flexibility and stability. The switching frequency is selectable between 650 kHz and 1.2 MHz and the minimum input voltage is 2.3 V . To control the inrush current at start-up a soft-start pin is available.

TPS61085 boost converter's novel topology using adaptive off-time provides superior load and line transient responses and operates also over a wider range of applications than conventional converters.
The selectable switching frequency offers the possibility to optimize the design either for the use of small sized components ( 1.2 MHz ) or for higher system efficiency ( 650 kHz ). However, the frequency changes slightly because the voltage drop across the $\mathrm{r}_{\mathrm{DS}(o n)}$ has some influence on the current and voltage measurement and thus on the on-time (the off-time remains constant).
The converter operates in continuous conduction mode (CCM) as soon as the input current increases above half the ripple current in the inductor, for lower load currents it switches into discontinuous conduction mode (DCM). If the load is further reduced, the part starts to skip pulses to maintain the output voltage.

## Design Procedure

The first step in the design procedure is to verify that the maximum possible output current of the boost converter supports the specific application requirements. A simple approach is to estimate the converter efficiency, by taking the efficiency numbers from the provided efficiency curves or to use a worst case assumption for the expected efficiency, e.g. $90 \%$.

1. Duty cycle, $D$ :

$$
\begin{equation*}
D=1-\frac{V_{I N} \cdot \eta}{V_{S}} \tag{1}
\end{equation*}
$$

2. Maximum output current, $I_{\text {OUT(max) }}$ :

$$
\begin{equation*}
I_{O U T(\max )}=\left(I_{L I M(\min )}-\frac{\Delta I_{L}}{2}\right) \cdot(1-D) \tag{2}
\end{equation*}
$$

3. Peak switch current in application, $I_{S W(\text { peak })}$ :

$$
\begin{equation*}
I_{S W(\text { peak })}=\frac{\Delta I_{L}}{2}+\frac{I_{O U T}}{1-D} \tag{3}
\end{equation*}
$$

with the inductor peak-to-peak ripple current, $\Delta I_{L}$

$$
\begin{equation*}
\Delta I_{L}=\frac{V_{I N} \cdot D}{f_{S} \cdot L} \tag{4}
\end{equation*}
$$

and

| $V_{I N}$ | Minimum input voltage |
| :--- | :--- |
| $V_{S}$ | Output voltage |
| $I_{\text {LIM(min) }}$ | Converter switch current limit (minimum switch current limit = 3.2 A) |
| $f_{S}$ | Converter switching frequency (typically 1.2 MHz or 650 kHz ) |
| $L$ | Selected inductor value |
| $\eta$ | Estimated converter efficiency (please use the number from the efficiency plots or $90 \%$ as an estimation) |

The peak switch current is the steady state peak switch current that the integrated switch, inductor and external Schottky diode has to be able to handle. The calculation must be done for the minimum input voltage where the peak switch current is the highest.

## Soft-start

The boost converter has an adjustable soft-start to prevent high inrush current during start-up. To minimize the inrush current during start-up an external capacitor connected to the soft-start pin SS and charged with a constant current, is used to slowly ramp up the internal current limit of the boost converter when charged with a constant current. When the EN pin is pulled high, the soft-start capacitor $\mathrm{C}_{\mathrm{ss}}$ is immediately charged to 0.3 V . The capacitor is then charged at a constant current of $10 \mu \mathrm{~A}$ typically until the output of the boost converter $\mathrm{V}_{\mathrm{S}}$ has reached its Power Good threshold (roughly $98 \%$ of $\mathrm{V}_{\mathrm{S}}$ nominal value). During this time, the SS voltage directly controls the peak inductor current, starting with 0 A at $\mathrm{V}_{S S}=0.3 \mathrm{~V}$ up to the full current limit at $\mathrm{V}_{\mathrm{SS}}=0.8$ V . The maximum load current is available after the soft-start is completed. The larger the capacitor the slower the ramp of the current limit and the longer the soft-start time. A 100 nF capacitor is usually sufficient for most of the applications. When the EN pin is pulled low, the soft-start capacitor is discharged to ground.

## Inductor Selection

The TPS61085 is designed to work with a wide range of inductors. The main parameter for the inductor selection is the saturation current of the inductor which should be higher than the peak switch current as calculated in the Design Procedure section with additional margin to cover for heavy load transients. An alternative, more conservative, is to choose an inductor with a saturation current at least as high as the maximum switch current limit of 3.2 A. The other important parameter is the inductor dc resistance. Usually, the lower the dc resistance the higher the efficiency. It is important to note that the inductor dc resistance is not the only parameter determining the efficiency. Especially for a boost converter where the inductor is the energy storage element, the type and core material of the inductor influences the efficiency as well. At high switching frequencies of 1.2 MHz inductor core losses, proximity effects and skin effects become more important. Usually, an inductor with a larger form factor gives higher efficiency. The efficiency difference between different inductors can vary between $2 \%$ to $10 \%$. For the TPS61085, inductor values between $3 \mu \mathrm{H}$ and $6 \mu \mathrm{H}$ are a good choice with a switching frequency of 1.2 MHz , typically $3.3 \mu \mathrm{H}$. At 650 kHz inductors between $6 \mu \mathrm{H}$ and $13 \mu \mathrm{H}$, typically $6.8 \mu \mathrm{H}$ are recommended. Possible inductors are shown in Table 1.
Typically, it is recommended that the inductor current ripple is below $35 \%$ of the average inductor current. Therefore, the following equation can be used to calculate the inductor value, $L$ :

$$
\begin{equation*}
L=\left(\frac{V_{I N}}{V_{S}}\right)^{2} \cdot\left(\frac{V_{S}-V_{I N}}{I_{\text {OUT }} \cdot f_{S}}\right) \cdot\left(\frac{\eta}{0.35}\right) \tag{5}
\end{equation*}
$$

with

| $V_{I N}$ | Minimum input voltage |
| :--- | :--- |
| $V_{S}$ | Output voltage |
| $I_{\text {out }}$ | Maximum output current in the application |
| $f_{S}$ | Converter switching frequency (typically 1.2 MHz or 650 kHz ) |
| $\eta$ | Estimated converter efficiency (please use the number from the efficiency plots or $90 \%$ as an estimation) |

Table 1. Inductor Selection

| $\stackrel{\mathrm{L}}{(\mu \mathrm{H})}$ | SUPPLIER | COMPONENT CODE | $\begin{gathered} \text { SIZE } \\ (\mathrm{L} \times \mathrm{W} \times \mathrm{H} \mathrm{~mm}) \end{gathered}$ | $\begin{gathered} \text { DCR TYP } \\ (\mathrm{m} \Omega) \\ \hline \end{gathered}$ | Isat (A) |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 1.2 MHz |  |  |  |  |  |
| 3.3 | Sumida | CDH38D09 | $4 \times 4 \times 1$ | 240 | 1.25 |
| 4.7 | Sumida | CDPH36D13 | $5 \times 5 \times 1.5$ | 155 | 1.36 |
| 3.3 | Sumida | CDPH4D19F | $5.2 \times 5.2 \times 2$ | 33 | 1.5 |
| 3.3 | Sumida | CDRH6D12 | $6.7 \times 6.7 \times 1.5$ | 62 | 2.2 |
| 4.7 | Würth Elektronik | 7447785004 | $5.9 \times 6.2 \times 3.3$ | 60 | 2.5 |
| 5 | Coilcraft | MSS7341 | $7.3 \times 7.3 \times 4.1$ | 24 | 2.9 |
| 650 kHz |  |  |  |  |  |
| 6.8 | Sumida | CDP14D19 | $5.2 \times 5.2 \times 2$ | 50 | 1 |
| 10 | Coilcraft | LPS4414 | $4.3 \times 4.3 \times 1.4$ | 380 | 1.2 |
| 6.8 | Sumida | CDRH6D12/LD | $6.7 \times 6.7 \times 1.5$ | 95 | 1.25 |
| 10 | Sumida | CDR6D23 | $5 \times 5 \times 2.4$ | 133 | 1.75 |
| 10 | Würth Elektronik | 744778910 | $7.3 \times 7.3 \times 3.2$ | 51 | 2.2 |
| 6.8 | Sumida | CDRH6D26HP | $7 \times 7 \times 2.8$ | 52 | 2.9 |

## Rectifier Diode Selection

To achieve high efficiency, a Schottky type should be used for the rectifier diode. The reverse voltage rating should be higher than the maximum output voltage of the converter. The averaged rectified forward current lavg, the Schottky diode needs to be rated for, is equal to the output current $I_{\text {Out }}$ :
$I_{\text {avg }}=I_{\text {OUT }}$

Usually a Schottky diode with 2 A maximum average rectified forward current rating is sufficient for most applications. The Schottky rectifier can be selected with lower forward current capability depending on the output current $I_{\text {out }}$ but has to be able to dissipate the power. The dissipated power, $P_{D}$, is the average rectified forward current times the diode forward voltage, $V_{\text {forward }}$.

$$
\begin{equation*}
P_{D}=I_{\text {avg }} \cdot V_{\text {forward }} \tag{7}
\end{equation*}
$$

Typically the diode should be able to dissipate around 500 mW depending on the load current and forward voltage.

Table 2. Rectifier Diode Selection

| CURRENT <br> RATING lavg | $\mathbf{V r}$ | $\mathbf{V}_{\text {forward } / \text { lavg }}$ | SUPPLIER | COMPONENT <br> CODE | PACKAGE <br> TYPE |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 750 mA | 20 V | $0.425 \mathrm{~V} /$ <br> 750 mA | Fairchild Semiconductor | FYV0704S | SOT 23 |
| 1 A | 20 V | $0.39 \mathrm{~V} / 1 \mathrm{~A}$ | NXP | PMEG2010AEH | SOD 123 |
| 1 A | 20 V | $0.52 \mathrm{~V} / 1 \mathrm{~A}$ | Vishay Semiconductor | B120 | SMA |
| 1 A | 20 V | $0.5 \mathrm{~V} / 1 \mathrm{~A}$ | Vishay Semiconductor | SS12 | SMA |
| 1 A | 20 V | $0.44 \mathrm{~V} / 1 \mathrm{~A}$ | Vishay Semiconductor | MSS 1 P 2 L | $\mu$-SMP (Low <br> Profile) |

## Setting the Output Voltage

The output voltage is set by an external resistor divider. Typically, a minimum current of $50 \mu \mathrm{~A}$ flowing through the feedback divider gives good accuracy and noise covering. A standard low side resistor of $18 \mathrm{k} \Omega$ is typically selected. The resistors are then calculated as:

$$
\begin{array}{ll}
R 2=\frac{V_{F B}}{70 \mu A} \approx 18 k \Omega \quad R 1=R 2 \cdot\left(\frac{V_{S}}{V_{F B}}-1\right) \\
V_{F B}=1.238 V & V_{\mathrm{FB}} \underbrace{v_{s}}_{\mathrm{R} 1} \mathrm{R} 2 \\
\equiv \tag{8}
\end{array}
$$

## Compensation (COMP)

The regulator loop can be compensated by adjusting the external components connected to the COMP pin. The COMP pin is the output of the internal transconductance error amplifier.
Standard values of $R_{\text {COMP }}=13 \mathrm{k} \Omega$ and $C_{\text {COMP }}=3.3 \mathrm{nF}$ will work for the majority of the applications.
See Table 3 for dedicated compensation networks giving an improved load transient response. The following equations can be used to calculate $R_{\text {COMP }}$ and $C_{\text {COMP }}$ :

$$
\begin{equation*}
R_{\text {COMP }}=\frac{110 \cdot V_{\text {IN }} \cdot V_{S} \cdot C_{\text {OUT }}}{L \cdot I_{\text {OUT }}} \quad C_{\text {COMP }}=\frac{V_{S} \cdot C_{\text {OUT }}}{7.5 \cdot I_{\text {OUT }} \cdot R_{\text {COMP }}} \tag{9}
\end{equation*}
$$

with

| $V_{I N}$ | Minimum input voltage |
| :--- | :--- |
| $V_{S}$ | Output voltage |
| $C_{\text {out }}$ | Output capacitance |
| $L$ | Inductor value, e.g. $3.3 \mu \mathrm{H}$ or $6.8 \mu \mathrm{H}$ |
| $I_{\text {OUT }}$ | Maximum output current in the application |

Make sure that $R_{\text {COMP }}<120 \mathrm{k} \Omega$ and $C_{\text {COMP }}>820 \mathrm{pF}$, independent of the results of the above formulas.

Table 3. Recommended Compensation Network Values at High/Low Frequency

| FREQUENCY | L | $\mathrm{V}_{\text {S }}$ | $\mathrm{V}_{\text {IN }} \pm \mathbf{2 0 \%}$ | $\mathrm{R}_{\text {comp }}$ | $\mathrm{C}_{\text {comp }}$ | Used $\mathrm{I}_{\text {Out }}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| High (1.2 MHz) | $3.3 \mu \mathrm{H}$ | 15 V | 5 V | $82 \mathrm{k} \Omega$ | 1.1 nF | 0.7A |
|  |  |  | 3.3 V | $75 \mathrm{k} \Omega$ | 1.6 nF | 0.5A |
|  |  | 12 V | 5 V | $51 \mathrm{k} \Omega$ | 1.1 nF | 0.9A |
|  |  |  | 3.3 V | $47 \mathrm{k} \Omega$ | 1.6 nF | 0.6A |
|  |  | 9 V | 5 V | $30 \mathrm{k} \Omega$ | 1.1 nF | 1.2A |
|  |  |  | 3.3 V | $27 \mathrm{k} \Omega$ | 1.6 nF | 0.8 A |
| Low (650 kHz) | $6.8 \mu \mathrm{H}$ | 15 V | 5 V | $43 \mathrm{k} \Omega$ | 2.2 nF | 0.7 A |
|  |  |  | 3.3 V | $39 \mathrm{k} \Omega$ | 3.3 nF | 0.5A |
|  |  | 12 V | 5 V | $27 \mathrm{k} \Omega$ | 2.2 nF | 0.9A |
|  |  |  | 3.3 V | $24 \mathrm{k} \Omega$ | 3.3 nF | 0.6A |
|  |  | 9 V | 5 V | $15 \mathrm{k} \Omega$ | 2.2 nF | 1.2A |
|  |  |  | 3.3 V | $13 \mathrm{k} \Omega$ | 3.3 nF | 0.8A |

Table 3 gives conservative $R_{\text {COMP }}$ and $C_{\text {COMP }}$ values for certain inductors, input and output voltages providing a very stable system. For a faster response time, a higher $R_{\text {Comp }}$ value can be used to enlarge the bandwidth, as well as a slightly lower value of $C_{\text {COMP }}$ to keep enough phase margin. These adjustments should be performed in parallel with the load transient response monitoring of TPS61087.

## Input Capacitor Selection

For good input voltage filtering low ESR ceramic capacitors are recommended. TPS61085 has an analog input IN . Therefore, a $1 \mu \mathrm{~F}$ bypass is highly recommended as close as possible to the IC from IN to GND.
One $10 \mu \mathrm{~F}$ ceramic input capacitors are sufficient for most of the applications. For better input voltage filtering this value can be increased. Refer to Table 4 and typical applications for input capacitor recommendations.

## Output Capacitor Selection

For best output voltage filtering a low ESR output capacitor like ceramic capcaitor is recommended. Two $10 \mu \mathrm{~F}$ ceramic output capacitors (or one $22 \mu \mathrm{~F}$ ) work for most of the applications. Higher capacitor values can be used to improve the load transient response. Refer to Table 4 for the selection of the output capacitor.

Table 4. Rectifier Input and Output Capacitor Selection

|  | CAPACITOR | VOLTAGE RATING | SUPPLIER | COMPONENT CODE |
| :---: | :---: | :---: | :---: | :---: |
| $\mathrm{C}_{\mathrm{IN}}$ | $10 \mu \mathrm{~F} / 1206$ | 16 V | Taiyo Yuden | EMK212 BJ 106KG |
| $\mathrm{IN}_{\mathrm{N}}$ bypass | $1 \mu \mathrm{~F} / 0603$ | 16 V | Taiyo Yuden | EMK107 BJ 105KA |
| $\mathrm{C}_{\text {Out }}$ | $10 \mu \mathrm{~F} / 1206$ | 25 V | Taiyo Yuden | TMK316 BJ 106KL |

To calculate the output voltage ripple, the following equation can be used:

$$
\begin{equation*}
\Delta V_{C}=\frac{V_{S}-V_{I N}}{V_{S} \cdot f_{S}} \cdot \frac{I_{O U T}}{C_{O U T}} \quad \Delta V_{C_{-} E S R}=I_{L(\text { peak })} \cdot R_{C_{-} E S R} \tag{10}
\end{equation*}
$$

with

| $\Delta V_{C}$ | Output voltage ripple dependent on output capacitance,output current and switching frequency |
| :--- | :--- |
| $V_{S}$ | Output voltage |
| $V_{I N}$ | Minimum input voltage of boost converter |
| $I_{S}$ | Converter switching frequency (typically 1.2 MHz or 650 kHz ) |
| $I_{\text {out }}$ | Output capacitance |
| $\Delta V_{C_{-} E S R}$ | Output voltage ripple due to output capacitors ESR (equivalent series resistance) |
| $I_{\text {SWPEAK }}$ | Inductor peak switch current in the application |
| $R_{C_{C} E S R}$ | Output capacitors equivalent series resistance (ESR) |

$\Delta \mathrm{V}_{\mathrm{C}_{-} \text {ESR }}$ can be neglected in many cases since ceramic capacitors provide low ESR.

## Frequency Select Pin (FREQ)

The frequency select pin FREQ allows to set the switching frequency of the device to 650 kHz (FREQ = low) or 1.2 MHz ( $F R E Q=$ high). Higher switching frequency improves load transient response but reduces slightly the efficiency. The other benefits of higher switching frequency are a lower output ripple voltage. The use of the 1.2 MHz switching frequency is recommended unless light load efficiency is a major concern.

## Undervoltage Lockout (UVLO)

To avoid mis-operation of the device at low input voltages an undervoltage lockout is included that disables the device, if the input voltage falls below 2.2 V .

## Thermal Shutdown

A thermal shutdown is implemented to prevent damages due to excessive heat and power dissipation. Typically the thermal shutdown threshold happens at a junction temperature of $150^{\circ} \mathrm{C}$. When the thermal shutdown is triggered the device stops switching until the temperature falls below typically $136^{\circ} \mathrm{C}$. Then the device starts switching again.

## Overvoltage Prevention

If overvoltage is detected on the FB pin (typically $3 \%$ above the nominal value of 1.238 V ) the part stops switching immediately until the voltage on this pin drops to its nominal value. This prevents overvoltage on the output and secures the circuits connected to the output from excessive overvoltage.

## APPLICATION INFORMATION

## General Boost Application Circuits



Figure 14. Typical Application, 3.3 V to $12 \mathrm{~V}\left(\mathrm{f}_{\mathrm{S}}=1.2 \mathrm{MHz}\right)$


Figure 15. Typical Application, 3.3 V to $12 \mathrm{~V}\left(\mathrm{f}_{\mathrm{S}}=\mathbf{6 5 0} \mathrm{kHz}\right)$


Figure 16. Typical Application, 3.3 V to $9 \mathrm{~V}\left(\mathrm{f}_{\mathrm{s}}=1.2 \mathrm{MHz}\right.$ )


Figure 17. Typical Application, 3.3 V to $9 \mathrm{~V}\left(\mathrm{f}_{\mathrm{S}}=650 \mathrm{kHz}\right.$ )


Figure 18. Typical Application with External Load Disconnect Switch

## TFT LCD Application Circuit



Figure 19. Typical Application 3.3 V to $9 \mathrm{~V}\left(\mathrm{f}_{\mathrm{S}}=1.2 \mathrm{MHz}\right)$ for TFT LCD with External Charge Pumps (VGH, VGL)

## WHITE LED Application Circuits



Figure 20. Simple Application (3.3V input $-\mathrm{f}_{\mathrm{sw}}=650 \mathrm{kHz}$ ) for wLED Supply (3S3P) (with Optional Clamping Zener Diode)


Figure 21. Simple Application (3.3V input - $\mathrm{f}_{\text {sw }}=650 \mathrm{kHz}$ ) for wLED Supply (3S3P) with Adjustable Brightness Control using a PWM Signal on the Enable Pin (with Optional Clamping Zener Diode)


Figure 22. Simple Application (3.3V input - $\mathrm{f}_{\text {sw }}=650 \mathrm{kHz}$ ) for wLED Supply (3S3P) with Adjustable Brightness Control using an Analog Signal on the Feedback Pin (with Optional Clamping Zener Diode)

## REVISION HISTORY

Changes from Original (June 2008) to Revision A Page

- Changed the circuit illustration value of $\mathrm{C}_{\text {Comp }}$ From: 1.6 nF To: 1.1 nF ..... 1
- Deleted Lead Temperature from the Abs Max table ..... 2
- Added a conditions statement and two new graphs (Max Load Current vs Input Voltage) to the Typical Characteristics graphs ..... 5
- Added three paragraphs of text to the Detailed Description - following the Block Diagram (Figure 13) ..... 8
- Changed the Design Procudures step 3 details following Equation 4 ..... 9
- Changed text in the Inductor Selection section "inductor current ripple is below $20 \%$ " to " inductor current ripple is below 35\%" ..... 10
- Changed Equation 8 ..... 11
- Added Used Iout to Table 3 ..... 12
- Added Equation 10 ..... 12
- Changed Figure 14 to Figure 18 ..... 13
- Changed the White LED Applications optional Zener connection for Figure 20 to Figure 22 ..... 16


## PACKAGING INFORMATION

| Orderable Device | Status ${ }^{(1)}$ | Package Type | Package Drawing | Pins | Package Qty | Eco Plan ${ }^{(2)}$ | Lead/ Ball Finish | MSL Peak Temp ${ }^{(3)}$ | Samples <br> (Requires Login) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| TPS61085DGKR | ACTIVE | VSSOP | DGK | 8 | 2500 | Green (RoHS \& no $\mathrm{Sb} / \mathrm{Br}$ ) | CU NIPDAU | Level-1-260C-UNLIM |  |
| TPS61085DGKRG4 | ACTIVE | VSSOP | DGK | 8 | 2500 | Green (RoHS \& no Sb/Br) | CU NIPDAU | Level-1-260C-UNLIM |  |
| TPS61085DGKT | ACTIVE | VSSOP | DGK | 8 | 250 | Green (RoHS \& no $\mathrm{Sb} / \mathrm{Br}$ ) | CU NIPDAU | Level-1-260C-UNLIM |  |
| TPS61085DGKTG4 | ACTIVE | VSSOP | DGK | 8 | 250 | Green (RoHS \& no $\mathrm{Sb} / \mathrm{Br}$ ) | CU NIPDAU | Level-1-260C-UNLIM |  |
| TPS61085PW | ACTIVE | TSSOP | PW | 8 | 150 | Green (RoHS \& no $\mathrm{Sb} / \mathrm{Br}$ ) | CU NIPDAU | Level-1-260C-UNLIM |  |
| TPS61085PWG4 | ACTIVE | TSSOP | PW | 8 | 150 | Green (RoHS \& no $\mathrm{Sb} / \mathrm{Br}$ ) | CU NIPDAU | Level-1-260C-UNLIM |  |
| TPS61085PWR | ACTIVE | TSSOP | PW | 8 | 2000 | Green (RoHS \& no $\mathrm{Sb} / \mathrm{Br}$ ) | CU NIPDAU | Level-1-260C-UNLIM |  |
| TPS61085PWRG4 | ACTIVE | TSSOP | PW | 8 | 2000 | Green (RoHS \& no $\mathrm{Sb} / \mathrm{Br}$ ) | CU NIPDAU | Level-1-260C-UNLIM |  |

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ACTIVE: Product device recommended for new designs
LIFEBUY: TI has announced that the device will be discontinued, and a lifetime-buy period is in effect.
NRND: Not recommended for new designs. Device is in production to support existing customers, but TI does not recommend using this part in a new design.
PREVIEW: Device has been announced but is not in production. Samples may or may not be available.
OBSOLETE: TI has discontinued the production of the device.
${ }^{(2)}$ Eco Plan - The planned eco-friendly classification: Pb-Free (RoHS), Pb-Free (RoHS Exempt), or Green (RoHS \& no Sb/Br) - please check http://www.ti.com/productcontent for the latest availability information and additional product content details.
TBD: The Pb-Free/Green conversion plan has not been defined.
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${ }^{(3)}$ MSL, Peak Temp. -- The Moisture Sensitivity Level rating according to the JEDEC industry standard classifications, and peak solder temperature.
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## OTHER QUALIFIED VERSIONS OF TPS61085 :

Automotive: TPS61085-Q1

NOTE: Qualified Version Definitions

- Automotive - Q100 devices qualified for high-reliability automotive applications targeting zero defects


## TAPE AND REEL INFORMATION

REEL DIMENSIONS


W1

TAPE AND REEL INFORMATION
*All dimensions are nominal

| Device | Package <br> Type | Package <br> Drawing | Pins | SPQ | Reel <br> Diameter <br> $(\mathbf{m m})$ | Reel <br> Width <br> W1 <br> $(\mathbf{m m})$ | A0 <br> $(\mathbf{m m})$ | B0 <br> $(\mathbf{m m})$ | K0 <br> $(\mathbf{m m})$ | P1 <br> $(\mathbf{m m})$ | W <br> $(\mathbf{m m})$ | Pin1 <br> Quadrant |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| TPS61085DGKR | VSSOP | DGK | 8 | 2500 | 330.0 | 12.4 | 5.3 | 3.4 | 1.4 | 8.0 | 12.0 | Q1 |
| TPS61085DGKT | VSSOP | DGK | 8 | 250 | 180.0 | 12.4 | 5.3 | 3.4 | 1.4 | 8.0 | 12.0 | Q1 |
| TPS61085PWR | TSSOP | PW | 8 | 2000 | 330.0 | 12.4 | 7.0 | 3.6 | 1.6 | 8.0 | 12.0 | Q1 |


*All dimensions are nominal

| Device | Package Type | Package Drawing | Pins | SPQ | Length (mm) | Width (mm) | Height (mm) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| TPS61085DGKR | VSSOP | DGK | 8 | 2500 | 367.0 | 367.0 | 35.0 |
| TPS61085DGKT | VSSOP | DGK | 8 | 250 | 210.0 | 185.0 | 35.0 |
| TPS61085PWR | TSSOP | PW | 8 | 2000 | 367.0 | 367.0 | 35.0 |



NOTES: A. All linear dimensions are in millimeters.
B. This drawing is subject to change without notice.

C Body length does not include mold flash, protrusions, or gate burrs. Mold flash, protrusions, or gate burrs shall not exceed 0.15 per end.
D Body width does not include interlead flash. Interlead flash shall not exceed 0.50 per side.
E. Falls within JEDEC MO-187 variation AA, except interlead flash.
PW (R-PDSO-G28)


NOTES: A. All linear dimensions are in millimeters. Dimensioning and tolerancing per ASME Y14.5M-1994.
B. This drawing is subject to change without notice.

C Body length does not include mold flash, protrusions, or gate burrs. Mold flash, protrusions, or gate burrs shall not exceed 0,15 each side.
D Body width does not include interlead flash. Interlead flash shall not exceed 0,25 each side.
E. Falls within JEDEC MO-153


NOTES: A. All linear dimensions are in millimeters. Dimensioning and tolerancing per ASME Y14.5M-1994.
B. This drawing is subject to change without notice.

C Body length does not include mold flash, protrusions, or gate burrs. Mold flash, protrusions, or gate burrs shall not exceed 0,15 each side.
D Body width does not include interlead flash. Interlead flash shall not exceed 0,25 each side.
E. Falls within JEDEC MO-153

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